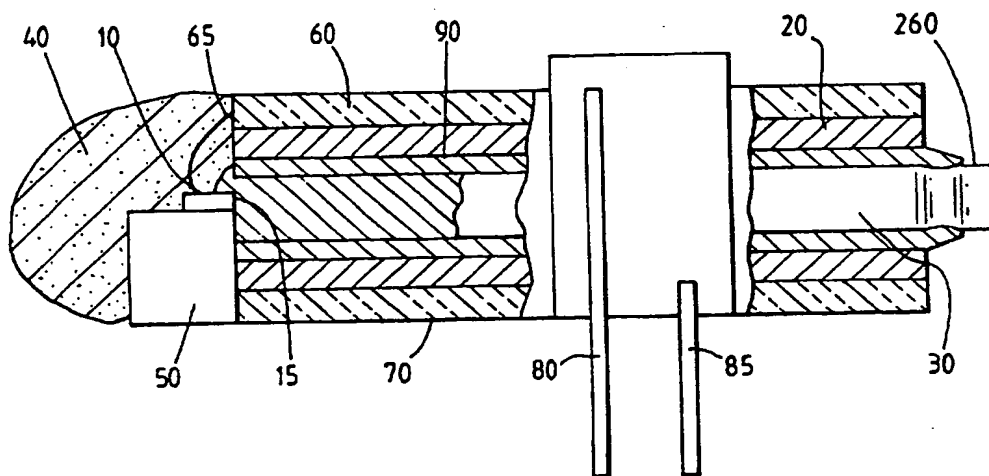


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(54) Title: PACKAGED OPTICAL DEVICE



## (57) Abstract

An optical device package comprises an optical device (10) held in optically coupled relationship with an optical fibre (260) by a ceramic ferrule (60). The optical device (10) is mounted on heatsink (50), the heatsink being mounted on the ferrule (60). The optical device (10) is accurately mounted in relation to the rim of the ferrule (60) such that insertion of the optical fibre (260) into the ferrule brings the optical fibre into optically coupled relationship with the optical device without the need for active alignment techniques. The optical device (10), in use, is encapsulated in silicon sealant (40) to seal the device from the effects of humidity.

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## PACKAGED OPTICAL DEVICE

The present invention relates to the packaging of an optical device in alignment with an optical fibre.

5       The importance of accurate alignment of an optical fibre with other components in optical devices is well known. In an optoelectronic device such as a transmitter or receiver, for example, alignment of an optical fibre with a laser or receiver chip is necessary to attain optimum coupling of light energy. This is especially true for transmitters, where, for example, good optical coupling permits  
10 a laser to be operated using minimum current, thus reducing the heat generated during lasing and extending the life of the laser. Thermal expansion problems inherent in transferring heat from the laser are also minimised and, for some applications, packaging costs can be reduced through elimination of the need for a thermoelectric cooler.

15       In fabrication, not only must the fibre be aligned in three co-ordinates for optimum coupling, but this alignment must also be fixed by a rigid securement and must not be altered by shrinkage forces during fixation or subsequent processing. For a single mode fibre, for example, final alignment must generally be held to within plus or minus one-half micrometer in dimensions radial to the fibre and to  
20 within one to two micrometers axially.

Conventionally, packages which incorporate environmentally sensitive components such as lasers, for example, are hermetically sealed to provide the component with a closed and protected environment. It is customary to introduce a communicating optical fibre into such packages via a suitable feed-through  
25 connection. In fabrication, the fibre is first inserted into the feed-through and the feed-through is secured to the package. The portion of fibre internal to the package is then aligned with the laser, or other component, and separately fixed in position. US 4615031, for example, discloses one such fabrication technique in which an anchorage clamp welded over the fibre inside the package is used to fix  
30 the alignment.

A similar approach to packaging an optical device is described in European patent application EP-A-0286319, where an optical fibre is hermetically sealed in a feed-through tube which is aligned with a laser through an aperture in a wall of a package. The feed-through tube has two supporting points, mounted on an inner

surface of the package, at which the tube can be manoeuvred to align it with the optical device. The fibre in the tube is actively optically aligned with the laser by powering up the laser and monitoring the level of light which passes along the fibre as the position of the fibre relative to the laser is altered. When the optimum  
5 alignment is achieved, the tube is secured in a fixed relationship to the laser. Using this approach requires that the package and the walls of the package do not deform due to changes in temperature, otherwise the fibre and the optical device could move out of optical alignment.

The cost of packaging optical devices is one of the key economic barriers  
10 to the deployment of a FTTH (fibre to the home) telecommunications network, since the devices are responsible for a significant proportion of the cost of the equipment to be installed in subscribers' premises. Of particular significance is the cost of optoelectronic components and assemblies such as, for example packaged semiconductor lasers. The largest component of the cost of, for example, a  
15 packaged semiconductor laser is incurred in the packaging of the device and not in the cost of the laser itself. One major cost for the packaging is for the special package or box required to house the laser and the hermetic sealing requirement associated with the package or box to protect the laser from the effects of humidity and other contaminants. Another contribution to the packaging cost is  
20 the need to use active fibre alignment techniques (i.e. techniques requiring active monitoring of laser light launched into the fibre during the alignment process) to align the optical fibre with the semiconductor laser.

For ease of explanation only, the following text refers to the specific case of aligning a laser with an optical fibre. It will nevertheless be appreciated by  
25 those skilled in the art that the invention is equally applicable to the alignment of optical fibres with other optical devices, such as detectors, modulators, amplifiers, filters, etc.

In accordance with a first aspect, the present invention provides a packaged semiconductor laser comprising: a semiconductor laser; an optical fibre;  
30 and a supporting member, the laser being carried by the supporting member, wherein the optical fibre is held in optically coupled relationship with the laser by the supporting member and the laser device is mounted externally of the supporting member.

Preferably, the optical fibre is bonded to the laser facet with an index matching adhesive, for example an epoxy based adhesive. The fibre may be bonded directly to the laser facet, in which case there would only be a thin layer of bonding adhesive between the fibre and the laser facet. Alternatively, the fibre  
5 may be bonded indirectly to the laser facet, for example by bonding a lens or other light transmitting means between the fibre and the laser facet. Attachment of the fibre to the facet, either directly or indirectly, cuts down on undesirable reflections between the facet and the fibre.

Alternatively, reflections between the facet and optical fibre may be  
10 minimised by known methods, for example by forming a lens on the end of the optical fibre, anti-reflection coating the end of the fibre, or polishing an angle on the fibre end. However, the method using adhesive has the advantage of adding strength to the assembly.

Preferably, the coupling efficiency between the laser facet and optical fibre  
15 is increased by using a high NA fibre, for example a fibre having a NA of greater than 0.25 (compared to a standard fibre having a NA of about 0.1), which has an acceptance angle which better matches the radiation beam angle, typically  $30^\circ \times 40^\circ$ , of the laser.

Alternatively, the alignment tolerance, and thus coupling efficiency  
20 between the laser facet and the optical fibre, is increased by using a large spot size laser (as described in our co-pending European patent application, number 94301309.4, filed on 24 February 1994) which has a large spot size output radiation beam which more closely matches the spot size of standard single mode telecommunications optical fibre (the spot size of a standard single mode  
25 telecommunications optical fibre is approximately  $10\mu\text{m}$  at a wavelength of  $1.55\mu\text{m}$ , whereas the spot size at the output facet of a typical double heterostructure semiconductor laser is  $1.0\mu\text{m}$  by  $1.5\mu\text{m}$ ). A large spot size semiconductor laser is fabricated with a waveguiding structure which has been modified to provide an output which is, typically, larger than a standard  
30 semiconductor laser and has less divergence.

Both a high NA fibre and a large spot size laser may be used in combination, however the inventors have shown that the use of a large spot size

laser with a standard telecommunications optical fibre provides extremely good coupling efficiency for the present invention of up to 66%.

One purpose of the supporting member is to hold the optical fibre in accurate optical alignment with the laser. This may be achieved in several ways, for example the supporting member may comprise a substrate, into one surface of which is formed a precision V groove reference surface. Preferably the precision V groove is formed by etching, especially by etching a mono-crystalline substrate. The optical fibre would be fixed into the V groove to maintain the alignment of the optical fibre. Additionally, this assembly may be strengthened by inverting another V grooved substrate over the fibre. The laser would be held in optically coupled relationship with the optical fibre against a second reference surface on the supporting member. Alternatively, the supporting member may be a precision ferrule into which the optical fibre is received to maintain its alignment. The internal surface of the ferrule bore provides a reference surface for the optical fibre. Other ways of holding the optical fibre will be apparent in view of the present disclosure.

In a preferred embodiment of the present invention, the supporting member is a ceramic ferrule with dimensions that are accurate enough for it to act as a base for the laser as well as providing a reference surface in the ferrule bore which provides an accurate support for the optical fibre. The rim of the ferrule is used as a reference surface to align the laser with the optical fibre.

Alternatively, the supporting member may be micro-machined into a silicon substrate, wherein the alignment of the laser on the supporting member is achieved by fabricating an alignment bump, typically comprising  $\text{SiO}_2$ , on a reference surface using lithographic mask and etch techniques, which guides the positioning of the laser relative to the end of the fibre which is held by the supporting member. The micro-machined substrate may provide a ferrule-like structure to receive the optical fibre, or it may be a V-grooved substrate for example.

Conventionally, a semiconductor laser needs a heatsink to dissipate heat generated during operation. Preferably, the supporting member itself acts as a suitable heatsink. Alternatively, the laser may be mounted on a device mount, which is itself attached to the supporting member, where the device mount acts as

a heatsink alone or in combination with the supporting member. A device mount heatsink would typically be of conventional type, for example one comprising a gold coated diamond onto which the laser is mounted. Typically, however, cost may be reduced by replacing the diamond with, for example, a diamond coated substrate, or a compound such as aluminium nitride or similarly heat-conducting material.

Preferably, electrical contacts for the semiconductor laser are provided as integral parts of the supporting member. Preferably the contacts are also in connection with PCB board pins (integral with the supporting member) to allow the whole packaged device to be mounted readily on a standard PCB arrangement.

In use, the laser is provided with some form of low cost protective cap in order to protect it from humidity and other contaminants. In a preferred embodiment of the present invention, the laser is coated with a silicone sealing gel which acts as such a cap. The inventors have shown that, surprisingly, silicone sealing gels are able to protect the laser from humidity and other contaminants sufficiently well, even for telecommunications applications (where the lifetime requirements are severe), that the lasers need not be contained in a hermetically sealed box, thus removing one of the main packaging cost overheads in known package production.

In embodiments of the invention, the protective cap, for example a silicon sealing gel, is index matching between the optical device and the optical fibre and acts in place of an index matching adhesive to bond the fibre to the device.

In accordance with a second aspect, the present invention provides a method of packaging a semiconductor laser, the method comprising, positioning and mounting a semiconductor laser on a supporting member, and fixing one end of an optical fibre to the supporting member, wherein the semiconductor laser is positioned to be external to the supporting member and in an optically coupled relationship with the optical fibre.

Preferably, the method further comprises the step of bonding the end of the optical fibre to a facet of the laser using an index matching adhesive. Preferably, the adhesive is an adhesive which is curable without the need for heating, for example a UV radiation curable adhesive.

In the case of a semiconductor laser, active alignment may be used to accurately align the semiconductor laser and device mount by turning the laser on and using the laser beam to position the components relative to, for example, the centre of a bore in the optical fibre supporting member, the laser beam, for example, impinging on an optical sensor when the correct position is achieved.

Alternatively, the laser may be passively positioned by a mechanical alignment system, and bonded into position. To obtain precise positioning, the laser is preferably bonded against alignment features, for example one or more groove(s), edge(s), shoulder(s) or bump(s), on the supporting member.

The laser may be manually positioned on the supporting member or, preferably, the laser may be positioned by an automatic placing and bonding machine which applies pressure to the laser to urge it against the alignment features on the supporting member during the bonding of the laser to the supporting member.

A drawback of passive alignment techniques is that the distance from an alignment edge of a laser body to the position of the laser mesa, critically affects the alignment of the laser with the optical fibre. For example, if the distance from the alignment edge to the active area can only be defined to micron accuracy, it may be impossible to optically align the optical fibre and the laser active area with sufficient accuracy by passive alignment techniques, particularly if the optical fibre is single mode.

Hitherto, techniques for fabricating accurately dimensioned laser chips have only achieved accuracies down to 1 micron. Typically, the dimensions of the substrate define the dimensions of the laser chip. These dimensions are typically defined by cleaving planes for single lasers cleaved from a bulk substrate. Therefore, the dimensions of known lasers are determined by how accurate the cleaving process is.

In accordance with a further aspect, the present invention provides a semiconductor laser comprising a semiconductor substrate and, deposited thereon, a plurality of epitaxial layers, wherein at least one of the epitaxial layers has an edge which defines an alignment edge of the laser.

Preferably, the alignment edge of the or each epitaxial layer is defined by a lithographic mask and etch procedure, which typically has an accuracy down to 0.25 $\mu$ m.

In a preferred embodiment the alignment edge is separate from the edge of the substrate which latter is defined by a cleave. Therefore, regardless of how accurate or inaccurate the dimensions of the cleaved substrate are, the dimensions of the laser are determined to sub-micron accuracy by the alignment edge defined by the or each epitaxial layer.

Preferably, the alignment edge on the laser co-operates with an alignment feature on a supporting member onto which the laser is to be mounted.

The alignment feature could be in the form of, for example, one or more bumps, or a ridge or ridges, on a reference surface of the supporting member, against which the alignment edge of the laser butts to maintain the laser in a required alignment in relation to the supporting member.

Preferably, the alignment feature on the supporting member is defined by a similar standard lithographic mask and etch procedure, using the same mask as for the alignment edge on the laser, to ensure sub-micron alignment between the finished alignment features on the supporting member and the alignment edge on the laser.

In accordance with a further aspect, the present invention provides a method of fabricating a semiconductor laser, the laser comprising a semiconductor substrate and deposited thereon a plurality of epitaxially grown layers, and an alignment edge, the method including the step of, forming at least one epitaxial layer having an edge determining the position of the alignment edge of the laser.

Conveniently, the epitaxial layer(s) edge, which defines the alignment edge, is formed using a standard lithographic mask and etch procedure suitable for determining the location of the edge of the epitaxial layer(s) to sub-micron accuracy.

Preferably, the epitaxial layer(s) which defines the alignment edge is separate from the edge of the semiconductor substrate, the edge of the substrate typically being defined by a cleave plane.

It will be appreciated that the foregoing references to a semiconductor laser apply, mutatis mutandis, to other semiconductor optical devices, for example detectors, modulators, amplifiers, filters, etc.

Embodiments of the present invention will now be described in detail, by way of example only, with reference to the accompanying drawings in which:

Figure 1 illustrates a first embodiment of the present invention;

Figures 2 and 3 illustrate a second embodiment of the present invention, in front elevation and exploded view respectively;

Figures 4a to 4i illustrate the steps involved in fabricating a semiconductor laser chip for use in the second embodiment;

Figure 5 shows a front elevation of a cleaved laser chip fabricated by the steps according to Figures 4a to 4i;

Figure 6 shows an alternative chip fabrication layout for the steps illustrated in Figures 4a to 4i;

Figure 7 shows in more detail an example of the second embodiment;

Figure 8 is a graph of coupling results achieved for packages according to the second embodiment; and

Figure 9 is a graph of a comparison between the heatsinking performance of the second embodiment of the invention and a standard diamond heatsink.

In Figure 1, the semiconductor laser 10 with a facet 15 is fixed to a heatsink 50 which is in turn fixed on a fibre supporting tube 20. The fixing means comprise a thermally conducting UV-curable adhesive. Such adhesive is used since there is no requirement to heat the device to form a bond as would be the case for solder joints or for thermo-compression bonding methods. The supporting tube 20 houses the optical fibre 30, so that the optical fibre is in an optically coupled alignment with the facet 15 of the laser 10. The optical fibre 30 is fixed into the supporting tube with an index matching UV-curable adhesive 90. Electrical contacts 60 and 70 are provided on the tube 20 to facilitate supply of electricity to the laser 10, via an electrical connection 65 and the heatsink 50, respectively. The electrical contacts 60 and 70 are connected to PCB board pins 80 and 85, respectively, which enable simple connection of the laser package to a PCB (not shown). The laser 10 is completely covered in a silicone gel cap 40, for

example Wacker (manufacturer) 905, to protect it from humidity and other contaminants.

The fibre support tube 20 is a precision manufactured ceramic ferrule, for example a ferrule available from Kyocera (Japan), which is manufactured to within 1 micron tolerance. The precision of the ferrule 20 enables it to act as a substrate for the whole laser package. Therefore, accurate positioning of the semiconductor laser 10 and the heatsink 50, in relation to the rim on the ferrule 20, enables the optical fibre 30 to be brought into optically coupled alignment with the laser facet 15 by simply inserting the optical fibre into the ferrule. In this way no active alignment is needed to align the optical fibre 30 with the facet 15.

Tests using this arrangement have been carried out and have provided the results shown in Table 1. For these tests, the optical fibre 30 was inserted into the ferrule 20 with the UV-curable adhesive 90. The laser 10 and the optical fibre 30 were aligned using active alignment in which the laser was powered-up and aligned with the fibre 30 on a standard alignment bench. Once aligned, the heatsink 50 was added to support the laser 10, and the heatsink was bonded to the ferrule 20 using UV-cured adhesive by exposing the arrangement to UV radiation. Measurements of optical coupling efficiency were taken at various stages of manufacture of each device, as shown in Table 1.

20

Laser Number	Pre Fixing	Heatsink Fixed	Epoxy Cure
1	55	55.0	41.3
2	44	47.1	45
3	42.5	42.5	42.1
4	54	52.7	51.3
Average			44.925

Table 1

In Table 1, 'Laser Number' identifies the laser on test, 'Pre Fixing' is the initial coupling efficiency due to active alignment, 'Heatsink Fixed' is the coupling

efficiency when the heatsink was added and 'Epoxy Cure' was the coupling efficiency after the device had been cured.

The results in Table 1 show that the average coupling efficiency is nearly 45%, using a large spot size laser having a maximum theoretical maximum efficiency of 66%.

Subsequent tests have been carried out using a very large spot size laser having a theoretical maximum efficiency of 76%. In these tests, coupling efficiencies in excess of 62% have been achieved. The applicants believe that coupling efficiencies approaching the theoretical maxima for the laser devices will be possible by fine-tuning the manufacturing process.

Figure 2 shows a second embodiment of a packaged semiconductor laser according to the present invention, which is shown in exploded view in Figure 3. The drawings show a silicon supporting member, or sub-mount, 200 which includes a SiO<sub>2</sub> alignment ridge 210 against which a semiconductor laser chip 220 is aligned. An advantage of using silicon for the sub-mount 200 is that it can be etched accurately taking advantage of its anisotropic properties to provide accurate etch depths and etch angles. A solder pad 230 is plated onto the sub-mount 200, onto which the laser chip 220 is mounted. The solder pad 230 provides thermal and electrical contact for the laser chip 220 as well as providing a fixing to hold the chip in place. The laser chip 220 has a precision alignment edge 240 which butts against the SiO<sub>2</sub> alignment ridge 210 to ensure accurate alignment of the laser chip 220 in relation to the sub-mount 200. A precision V groove 250, which is etched into the sub-mount 200, extends from one edge of the sub-mount 200 to the edge of the laser chip 220. The V groove 250 has a depth such that an optical fibre 260 received in the V groove optically aligns with the laser chip 220. The V groove 250 is formed using known masking and anisotropic etching techniques. The optical fibre 260 is bonded into the V groove 250 using an index matching UV curable adhesive or other suitable known adhesive.

As indicated previously, it is desirable to be able to employ a passive rather than an active alignment technique. Passive alignment techniques can be used with the above identified embodiments provided that the laser chip alignment edge is an accurately defined distance from the light emitting area of the laser

facet, or mesa. Hitherto, techniques for fabricating accurately dimensioned laser chips have only achieved accuracies down to 1 micron. However, the inventors have developed a technique for fabricating laser chips with sub-micron dimension accuracy. This method finds particular application in fabricating lasers for use in  
5 the present invention, but is also of more general application.

The process for fabricating sub-micron accuracy, pn diode laser chips is described, by way of example only, with reference to Figures 4a to 4i. Figure 4a shows a InP substrate 400, with two epitaxially grown surface layers 402 and 404 and a layer of silicon dioxide ( $\text{SiO}_2$ ), which has been etched to form an outline from  
10 which the laser chip is to be fabricated. In Figures 4a to 4i, the layers 402 and 404 (shown inset in Figure 4a and 4b) are represented as a single, un-shaded layer for clarity.

The substrate 400 is typically S-doped to a level of between  $3 \times 10^{18} \text{cm}^{-3}$  and  $1 \times 10^{19} \text{cm}^{-3}$ . The layers comprise an  $\text{In}_w\text{Ga}_x\text{As}_y\text{P}_z$  quaternary active (Q-active)  
15 layer 402, typically  $0.15 \mu\text{m}$  thick, which is capped with a protective InP layer 404, typically  $50 \text{nm}$  thick, doped with Zn to a level of around  $5 \times 10^{17} \text{cm}^{-3}$ . The wavelength at which the laser chip eventually lases is determined by the ratio of component amounts in the Q-active layer. Typically, to lase at  $1300 \text{nm}$ , the component ratios for w:x:y:z would be:- 0.74:0.26:0.56:0.44, or at  $1550 \text{nm}$ , the  
20 ratios would be:- 0.61:0.39:0.83:0.17. The etching was carried out, using standard photolithographic and etching procedures, by coating the substrate in  $\text{SiO}_2$  410 and covering the  $\text{SiO}_2$  with a standard positive photo-resist, typically a chromium coated quartz glass, to define outline areas for a buried heterostructure (BH) laser mesa 420 ( $\sim 3.5 \mu\text{m}$  wide) and V groove apertures 430 ( $\sim 5.0 \mu\text{m}$  wide)  
25 on the substrate 400. The outline was firstly etched into the  $\text{SiO}_2$ , 410 typically using a standard reactive ion etch (RIE), for example  $\text{CF}_4$  plasma @  $10 \text{mT}$  and  $150 \text{W}$ , or a wet etch in HF based etchant, for example 10:1 buffered HF (isoclean grade @  $20^\circ\text{C}$ ). The remaining  $\text{SiO}_2$  410 was then used as a mask to etch the underlying semiconductor 400 to a depth of approximately  $1.0 \mu\text{m}$ , using a suitable  
30 crystallographic etchant, for example a crystallographic wet etch of 14:1:9 {DI  $\text{H}_2\text{O}:(17:1 \text{HBr}:\text{Br}_2):\text{HBr}$ } @  $5^\circ\text{C}$ , or an RIE of  $\text{CH}_4/\text{H}_2$  plasma @  $70 \text{mT}$  and  $200 \text{W}$ . The remaining photo-resist was removed using, typically, acetone followed by concentrated sulphuric acid. At this stage, the distance from the centre of the

laser mesa 420 to the edge of the V groove aperture 430 is defined by the accuracy of the photolithographic process, which is typically within  $\pm 0.25\mu\text{m}$  accuracy.

Figure 4b shows the second stage of fabrication in which the laser mesa 420 is protected with a suitable protective resist 450, typically chromium coated quartz glass, whilst the remaining  $\text{SiO}_2$  410 is removed with  $\text{CF}_4$  from plateau regions 460 left after the first stage of photolithography, leaving the InP cap layer 404 exposed. First and second stages of overgrowth are shown in Figures 4c and 4d in which a conventional blocking structure 470 and contact layers 480 are epitaxially grown onto the structure respectively.

The blocking layer comprises two layers, one of p-InP 472, typically  $0.5\mu\text{m}$  thick, doped with Zn to a level of  $5 \times 10^{17}$  and one of n-InP 474, typically  $0.4\mu\text{m}$  thick, doped with S to a level of  $1-2 \times 10^{18}$ . The blocking layers are arranged in reverse bias to the n-type and p-type layers of the pn diode laser chip (usually with the n-type layer on top).

The contact layer 480 comprises two layers, one of Zn-doped InP 482 (which in fact comprises two layers:- a lower layer  $0.7\mu\text{m}$  thick, doped to a level of  $5 \times 10^{17}$ , and an upper layer  $0.7\mu\text{m}$  thick, doped to a level of  $1-2 \times 10^{18}$ ). The other contact layer 484 is of InGaAs,  $0.1\mu\text{m}$  thick, doped to a level of  $> 4 \times 10^{19}$ , to provide a near metallic p + + surface layer for electrical contact.

The InGaAs contact layer 484 is then patterned lithographically (Figure 4e) to reduce the current path and minimise capacitance effects by etching areas of the contact layer away. This is achieved using an  $\text{SiO}_2$  mask 486 and etching the InGaAs in a wet etch, comprising:-  $\text{H}_2\text{SO}_4$  (1 part);  $\text{H}_2\text{O}_2$  (1 part) and  $\text{H}_2\text{O}$  (25 parts).

In practice, the patterning removes all but a small area of the InGaAs layer 484, leaving an area typically  $15\mu\text{m}$  wide above the mesa 420.

The next stage is trenching, as shown in Figure 4F, where trenches 490 are etched either side of the laser mesa 420, using a suitable mask 492, typically  $\text{SiO}_2$ , and etchant, for example a wet etch, comprising:-  $\text{H}_3\text{PO}_4$  (4 parts) and  $\text{HCl}$  (1 part). The operating speed of a BH semiconductor laser is dependant on many factors, the capacitance of the blocking structure being one of the more important. The trenches isolate the mesa 420 from capacitance effects due to the overall

blocking structure 470, thus permitting high speed laser operation in the absence of such capacitance effects.

After the trenching stage, the masking  $\text{SiO}_2$  492 is removed from the slice and the slice is re-coated in a fresh layer of  $\text{SiO}_2$  502. A contact window  $\sim 10\mu\text{m}$  wide is then opened over the laser mesa to allow electrical contact to be made to the laser. During this process, windows over the V groove apertures 430 are again opened.

Figure 4g shows formation of p side contact metalisation (TiAu) for the electrical contact windows 500 and the protection of the windows with a layer of resist 510, for example a standard positive photo-resist such as Hoechst AZ5214E, as the mask for a further patterning step. The Au layer is etched in a wet etchant based on KI and the Ti is etched by RIE in a  $\text{CF}_4$  plasma using standard conditions. The same metalisation is plated onto the bottom of the slice (not shown) to form the n side contact, after the slice has been thinned to  $\sim 90\mu\text{m}$  using a standard wet etchant (Br/methanol).

Note: during the V groove etching (described below), using HBr, the resist mask used to pattern the p metal is left on the metal to act as a protective layer and is removed after the V grooves have been etched.

Figure 4h shows how the V grooves 520 are further etched using HBr which erodes the InP substrate but not the Q-layer 402. The apertures 430 at the mouths of the V grooves 520, and hence the distance between the edge of the V groove and the mesa 420, are accurately defined to within  $1\mu\text{m}$  by the previously etched Q-layer 402 which was defined in the first stage (Figure 4a). The V groove 520 profile has a diamond shape, resulting from crystallographic etching properties of HBr in the  $\langle 110 \rangle$  InP crystal direction. Figure 4i shows the resulting structure with cleave planes 530 defined at the bottoms of the V grooves 520.

Once cleaved, as shown in Figure 5, this structure provides two possible alignment mechanisms for the laser chip. Firstly, there is the Q-edge 240, which potentially provides sub-micron accuracy between the centre of the laser mesa 420 and the Q-edge 240. Secondly there is the cleavage plane 530 emanating from the bottom of the V groove 520, which should be accurate to within 1 micron.

Alternative cleaving arrangements used to cleave laser chips can take advantage of the fact that the cleaving mechanism is no longer an essential feature of the alignment process, if the Q-edge (which is not cleaved) is used for alignment.

5        Thus, Figure 6 shows much wider apertures 435 (~50µm wide) which can easily be fabricated on the semiconductor. In this case the laser chips would be separated by cleaving in the conventional way using a diamond scribing tool 550, however the accurate non-cleaved alignment edge would then be the one used for actual alignment purposes.

10        In practice the relevant parts of the same mask would be used for etching the sub-mount and the laser chip substrate, to ensure that they matched in terms of accurately aligning the laser chip with the sub-mount.

Figure 8 shows in more detail an example of the invention described above in relation to Figures 2 and 3. A 1550nm Fabry-Perot laser 220 is shown mounted  
15        on a micro-machined silicon optical bench 200. The laser 220 is a large spot size laser which has an 8 well compressive strained active layer, the planar design having been previously reported in the Applicant's prior patent application number 94301309.4.

The first stage of the photolithography for the laser is used to define both  
20        the passive guide (not shown) of the large spot size laser and channels (not shown) at the edge of the device which define scribe lanes 435 by which multiple lasers fabricated on a common substrate can be separated. A precision cleaved edge 240 of a scribe lane may be defined by this method to an accuracy of about  $\pm 0.2\mu\text{m}$ .

25        In this embodiment, scribe lanes 435 buried by further layers resulting from subsequent fabrication steps are exposed and the scribe lanes etched using 4:1  $\text{H}_3\text{PO}_4\text{:HCL}$ . The result of this etching is a substantially U-shaped channel approximately 20µm deep and 5µm wide, the precision cleaved edges 240, or top corners, of which are defined by a 1.1µm quaternary of the passive guide of the  
30        laser. The fabricated devices are cut from a common substrate into devices 1.1mm long by 300µm wide (defined by the scribe lanes). The length of the device comprises 340µm of un-tapered active region, a 460µm tapered region and a 300µm passive region.

Optimised coupling measurements of a number of devices, manufactured according to the above method, mounted on conventional headers yielded coupling efficiencies of up to 62% to cleaved ended single mode optical fibre.

In Figure 8, the laser device 220 is mounted on the silicon optical bench 200 with an intervening solder bond-pad 230 which provides thermal and electrical contact between the laser 220 and the silicon optical bench 200. The laser 220 is aligned by butting the precision quaternary edge 240 against a silica ( $\text{SiO}_2$ ) alignment stop 210, said stop having previously been formed on the bench as described below.

10 Silicon micro-machining techniques are used to fabricate the silicon optical bench 200 on which the laser 220, is passively aligned. The main features of the silicon optical bench 200 are a V-groove 250 for fibre attachment and a silica stop 210 against which the precision cleaved edge 240 of the laser chip 220 is aligned. The silica stop 210 is  $15\mu\text{m}$  high and is formed by plasma enhanced chemical vapour deposition and etched by a combination of reactive ion etching and wet  
15 chemical etching. The solder bond-pad 230 is formed by e-beam evaporation of 50nm titanium, 200nm platinum and 200nm gold, and is patterned using lift-off.  $3\mu\text{m}$  gold-tin solder is then thermally evaporated onto the resulting metal bond-pad 230, and is also patterned using lift-off. The fibre V-groove 250 is formed by  
20 anisotropic etching of  $\langle 100 \rangle$  silicon wafers using ethylene diamine and pyrocatechol, using a silicon nitride mask. The V-groove 250 has a depth such that the core of a suitable single mode optical fibre 260 substantially optically aligns with the laser. The exact depth of the V-groove 250 in practice is determined by experiment with the etchants, silicon substrate and optical fibre 260  
25 used.

A groove 710 is etched perpendicular to the V-groove 250 to enable glue used to hold the fibre 260 in place to flow freely underneath the fibre. Also, a shallow saw-cut 700 is made at the end of the V-groove 250 adjacent the laser 220 to remove the sloping end face of the V-groove, which remains after the V-  
30 groove is etched. This to allows the fibre 260 to be brought close to the laser 220 facet.

Fabrication of the package is as follows. The laser 220 is bonded against the silica alignment stop 210 on the silicon bench 200 using a conventional laser

die bonder. A cleaved single mode optical fibre 260 is then laid in the V-groove 250 on the optical bench 200 and is glued in place with a UV-cured adhesive. Further to this, a lid (not shown) made from a piece of silicon with an etched V-groove is applied over the top of the fibre 260 to clamp the fibre firmly in place and to provide rigidity.

A number of packaged laser devices according to Figure 7 have been manufactured as described above. Also, a number of laser chips from the same wafer were separated and were bonded, junction side down, on diamonds on conventional headers for the purposes of performance comparison. These diamond-mounted arrangements were found to have very uniform characteristics. Their output powers at 50mA and 20°C, were found to be in the range of 5-6mW.

The coupling efficiencies of the devices on the silicon optical benches were estimated by comparing the output power in the single mode fibre at 50mA and 20°C, to the average value of 5.5mW. Using this technique, coupling efficiencies as high as 55% have been calculated.

As shown in Figure 8, reproducible yields of packaged devices according to the invention have been demonstrated, mainly having coupling efficiencies greater than 30%, but significantly there is a substantial yield at greater than 50% efficiency.

As can be seen from Figure 9, the thermal properties of the lasers on the silicon bench compare favourably with the test devices bonded on diamonds. It is suggested that the larger footprint of the silicon bench compared with the diamond mounting compensates for the lesser thermal conductivity of the silicon.

Initial assessment of the modulation capability of a device according to this invention shows back to back bit error rate measurements indicating that the device is capable of modulation at rates in excess of 300MBit/s.

The skilled person will appreciate that the combination of low-cost packaging, high coupling efficiency and bandwidth in the packaged laser according to the present invention shows this to be a viable technology for fibre-to-the-home (FTTH).

While the laser chip fabrication technique described above finds particular application in the method of forming a packaged semiconductor laser

device according to the present invention, it will be apparent that the technique finds important application in the general field of semiconductor device fabrication and alignment. In particular, the method is not limited to the steps described above for fabricating a standard pn diode laser. The method finds application in  
5 the fabrication of other types of laser, for example MQW lasers or large spot size lasers, or indeed any type of semiconductor device which requires sub-micron alignment. Thus the precise details of layer composition, doping, thickness and of overall device dimensions are given by way of example only. Other devices, whether laser or otherwise, according to this aspect of the invention will typically  
10 have very different characteristics to those described above. In particular, the quaternary layer which provides the non-cleaved alignment edges also provides the device's active layer. In other devices, the equivalent layer might well not be a quaternary, possibly being a ternary, binary or other composition. Moreover, the layer which provides the non-cleaved alignment edge might be one other than that  
15 which provides the device's active layer - indeed the device may have no readily identifiable active layer. Nevertheless, the application of this aspect of the present invention to the easing of alignment problems will be clear to those skilled in the art.

## CLAIMS

1. A semiconductor device incorporating an alignment feature, said device comprising a semiconductor substrate and deposited thereon one or more device  
5 layers, wherein at least one of the device layers has a boundary defined by a photolithographic mask and etch process and wherein said boundary defines said alignment feature.
2. A semiconductor device according to claim 1, the device including an  
10 active region defined in one or more device layers, wherein said alignment feature is defined by at least one of the same one or more layers.
3. An optical device package comprising:
  - a) an optical fibre;
  - 15 b) an optical device having an alignment feature defined in accordance with claim 1 or 2; and
  - c) an optical fibre supporting member, the optical fibre supporting member providing a reference surface with respect to which the alignment feature of the optical device is positioned to effect alignment between the device and the optical  
20 fibre.
4. An optical device package according to claim 3, wherein the supporting member and the optical device are in thermal contact with one another, such that the supporting member acts as a heatsink for the optical device.
- 25 5. An optical device package according to claim 3 or claim 4, wherein the supporting member has a supporting V groove providing a reference surface to receive an optical fibre.
- 30 6. An optical device package according to claim 5, wherein the supporting member further comprises a strengthening member having a strengthening V groove, the strengthening V groove being arranged to overlie the supporting V groove to form a substantially square section bore to contain said optical fibre.

7. An optical device package comprising an optical device, an optical fibre and a support member, said support member providing a bore into which the optical fibre is received and a reference surface in relation to which said optical device is mounted to effect alignment with the end of said optical fibre received in said bore.

8. An optical device according to claim 7, wherein the device is mounted on a heatsink and the heatsink is mounted on said reference surface.

10

9. An optical device package according to claim 7 or claim 8, wherein electrical contacts to power the optical device are provided on the supporting member.

15 10. An optical device package according to any one of claims 7 to 9, wherein the supporting member is further provided with PCB pins which are in electrical contact with respective electrical contacts.

11. An optical device package according to any one of claims 7 to 10, wherein  
20 the supporting member comprises a ferrule.

12. An optical device package according to claim 11, wherein the rim of the ferrule provides the reference surface.

25 13. An optical device package according to claim 11 or claim 12, wherein the optical fibre is received in the bore of the ferrule, which bore holds the optical fibre in optically coupled alignment with the optical device.

14. An optical device package according to any one claims 3 to 13, wherein  
30 the optical device has a silicone gel coating.

15. An optical device package according to claim 14, wherein the silicone gel is index matching and forms a bond between the optical device facet and the end of the optical fibre.
- 5 16. An optical device package according to any one of claims 3 to 14, wherein the end of the optical fibre is bonded to the optical device facet using an index matching adhesive.
17. An optical device package according to any one of claims 3 to 16, wherein  
10 the optical fibre has a numerical aperture greater than 0.25.
18. An optical device package according to any one of claims 3 to 17, wherein the optical device is a semiconductor laser having a waveguiding structure which has been modified to provide an output which substantially matches the  
15 fundamental mode spot size of a single mode optical fibre.
19. A method of fabricating a semiconductor device, the method incorporating steps to define an alignment feature for said device, said steps including defining by a photolithographic mask and etch process a boundary in one or more layers of  
20 material forming part of the device, wherein said boundary defines said alignment feature.
20. A method according to claim 19, wherein an active region is defined in one or more layers of material forming part of the device, wherein said alignment  
25 feature is defined by at least one of the same one or more layers.
21. A method according to claim 20 or claim 21, including the steps of:
- a forming a layer of material on a first surface of the device; and
  - b masking said layer of material and etching away unmasked areas to  
30 provide a second surface lower than the first surface,
- wherein the edge of the first surface above said second surface provides said boundary and defines said alignment feature.

22. A method according to any one of claims 19 to 21, wherein the or at least some of the layers of material is or are deposited by epitaxial growth.
23. A method of packaging an optical device, said method comprising
- 5 a) mounting an optical fibre on a support member, said support member providing a reference surface for said optical fibre; and
- b) mounting on said support member an optical device having an alignment feature defined in accordance with claim 1 or 2 such that said alignment feature is urged against a reference surface provided on said support member to effect
- 10 alignment between the device and the optical fibre.
24. A method according to claim 23, wherein the optical fibre is bonded to the support member using a UV-cured adhesive.
- 15 ~~25~~. A method of packaging an optical semiconductor device having an alignment feature provided in accordance with claim 1 or claim 2, the method comprising the steps of:
- a) mounting an optical fibre on an optical fibre supporting member, the supporting member having a first reference surface, against which the optical fibre
- 20 is fixed;
- b) positioning the alignment feature of the optical device against a second reference surface of the supporting member;
- c) securing the device and the fibre together in optically coupled relationship without active alignment; and
- 25 d) encapsulating the device to provide a non-hermetic package.

Fig.1.

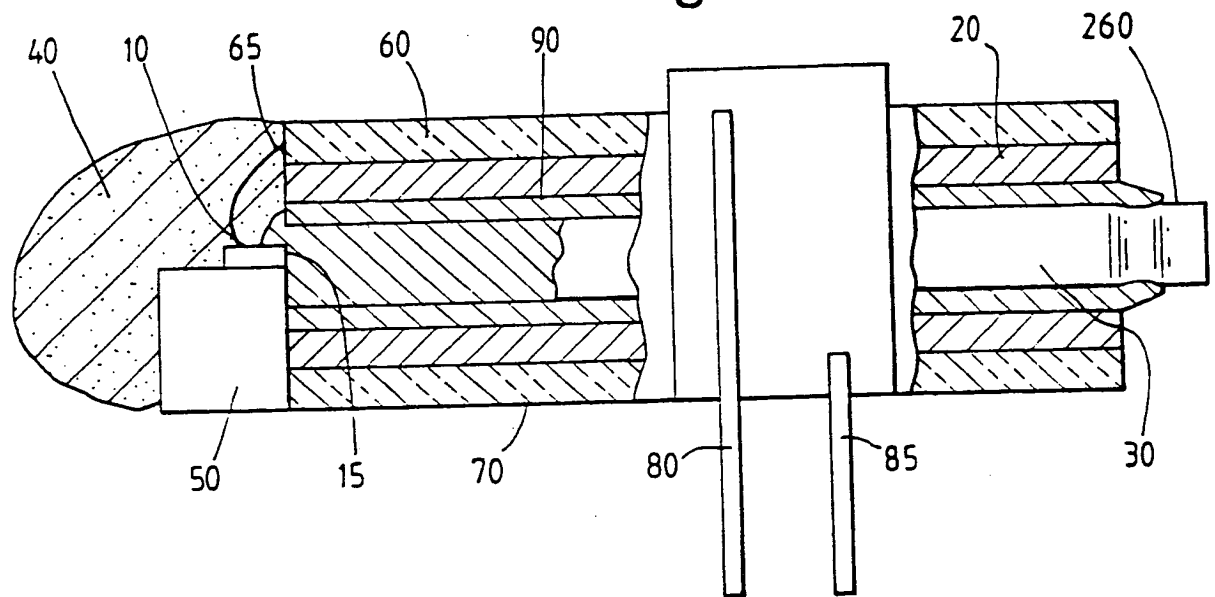


Fig.2.

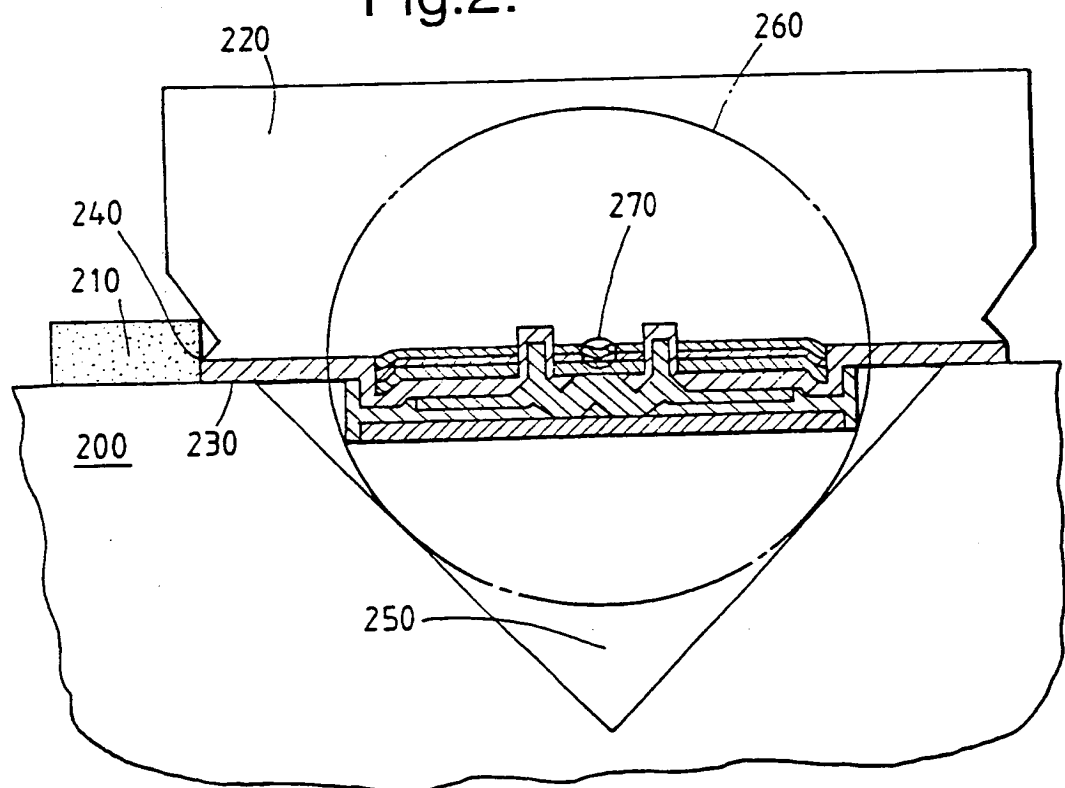


Fig.3.

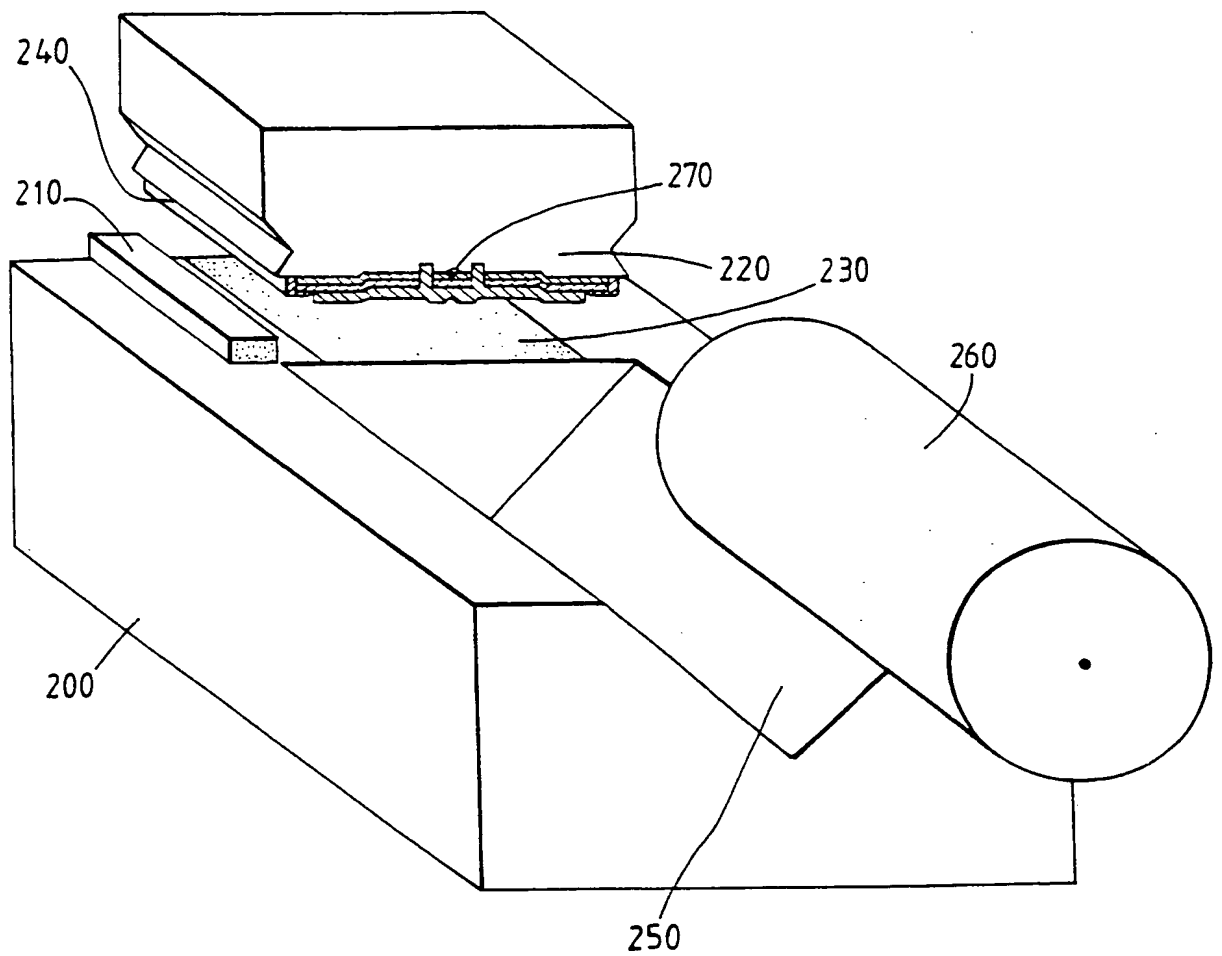


Fig.4a.

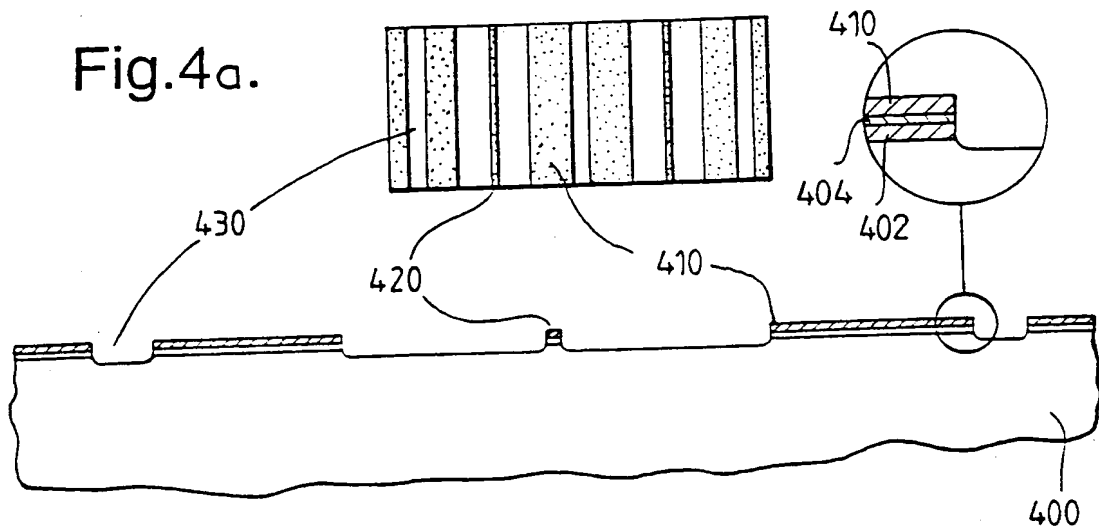


Fig.4b.

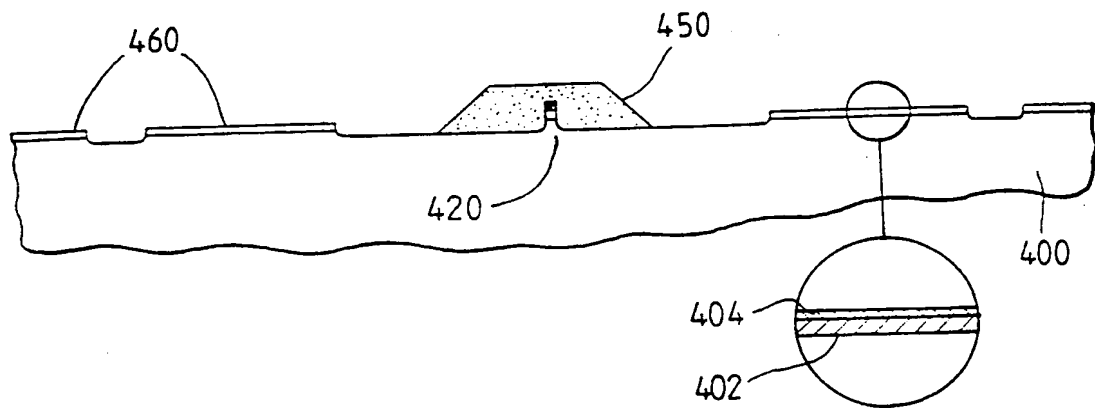


Fig.4c.

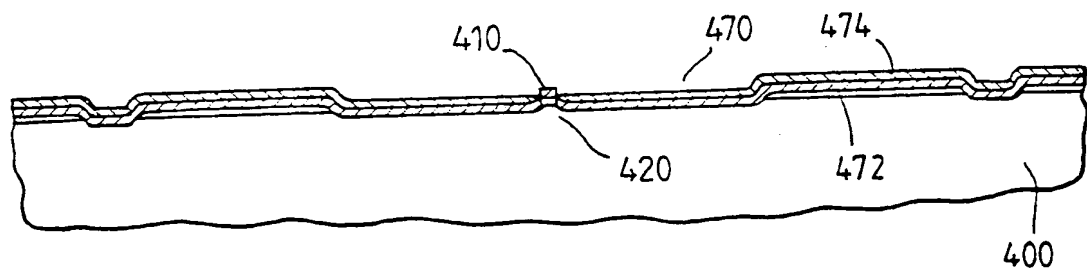


Fig.4d.

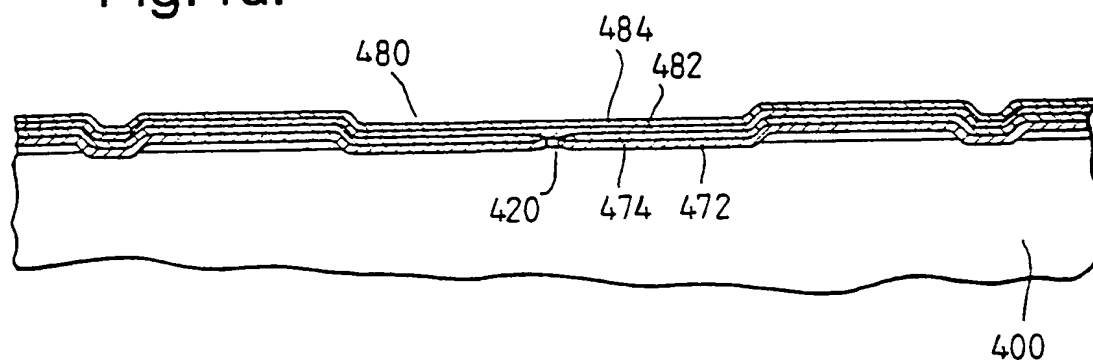


Fig.4e.

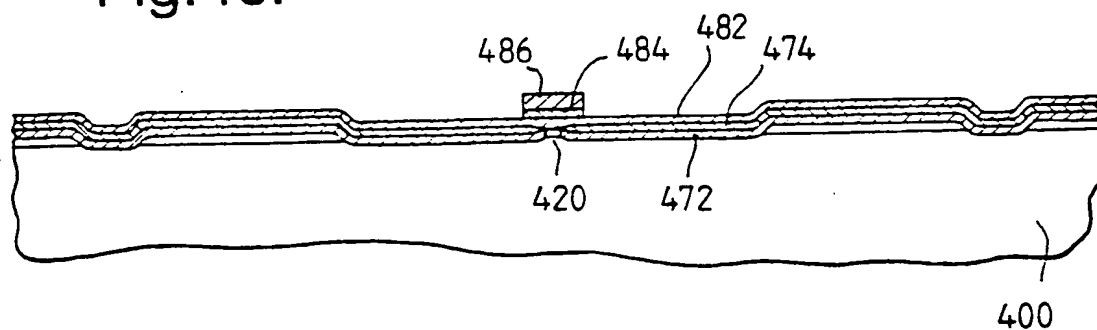


Fig.4f.

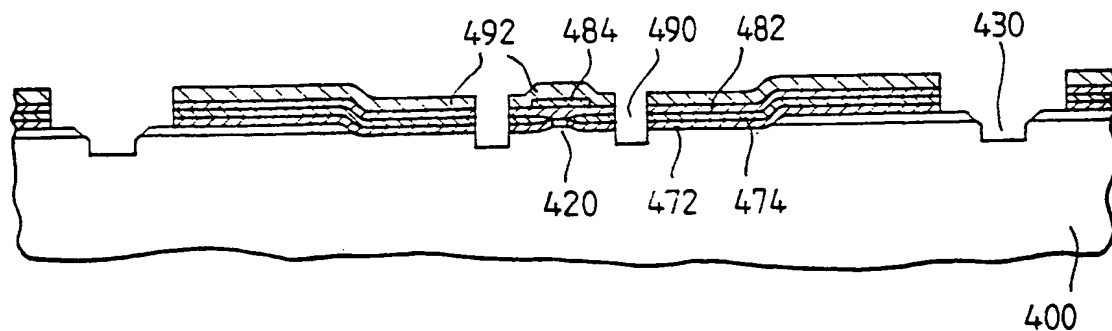


Fig.4g.

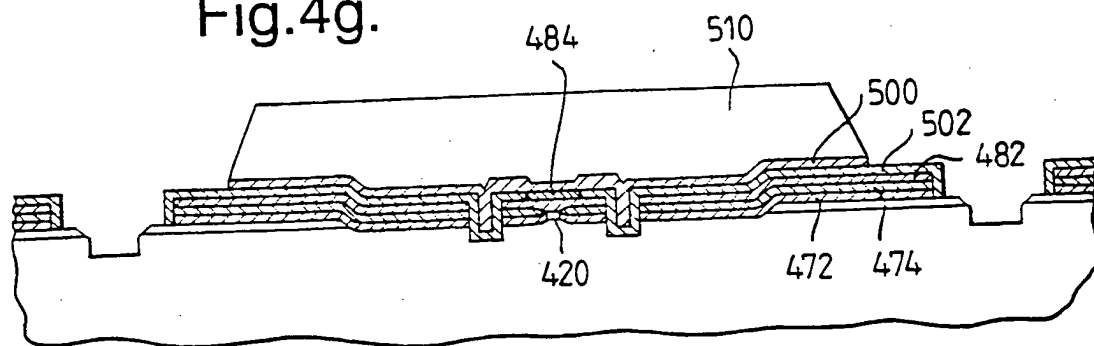


Fig.4h.

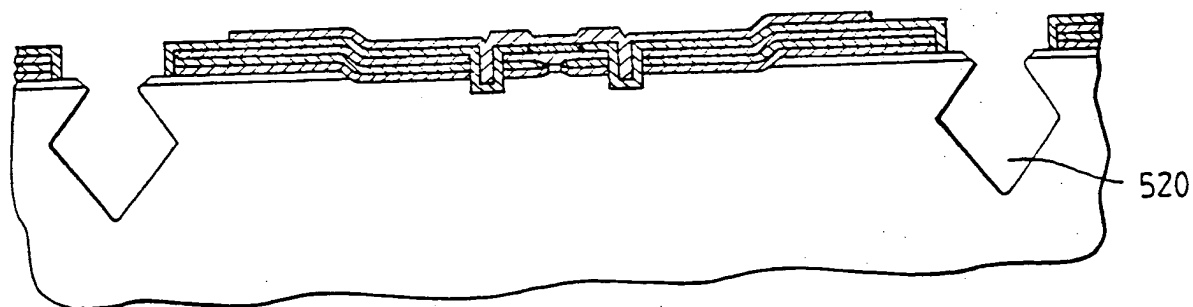


Fig.4i.

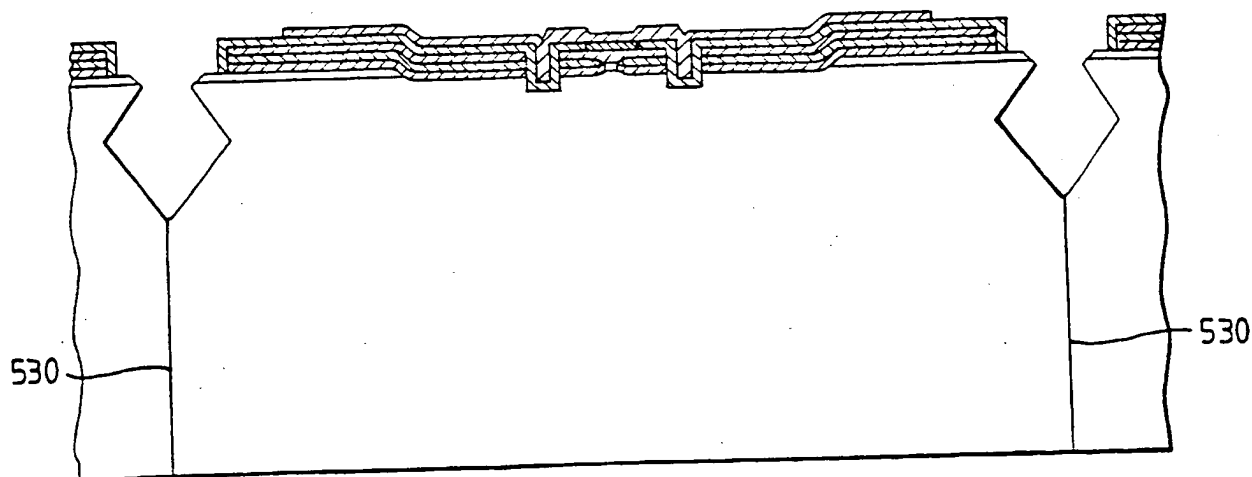


Fig.5.

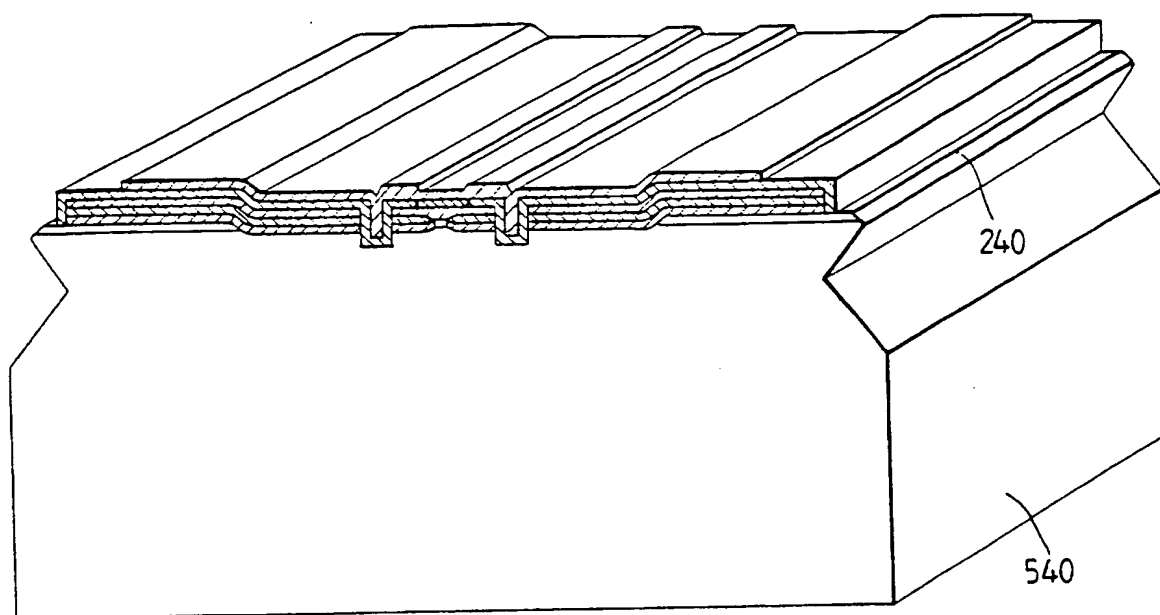
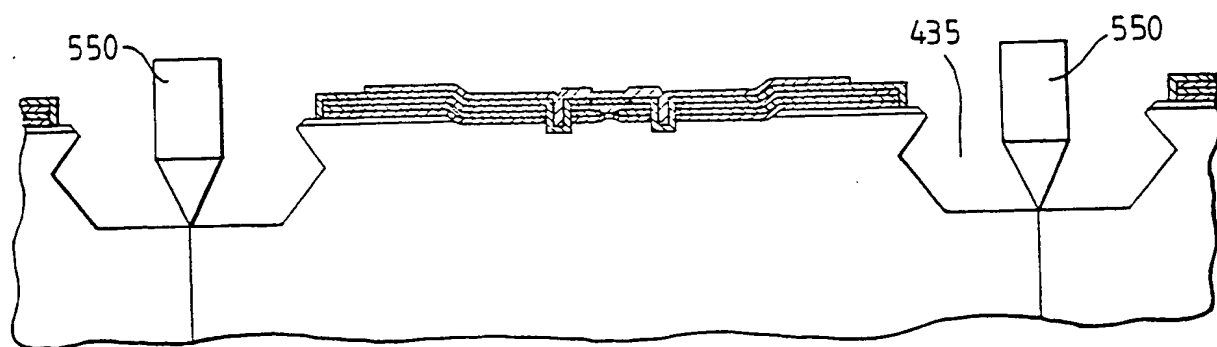


Fig.6.



7/8

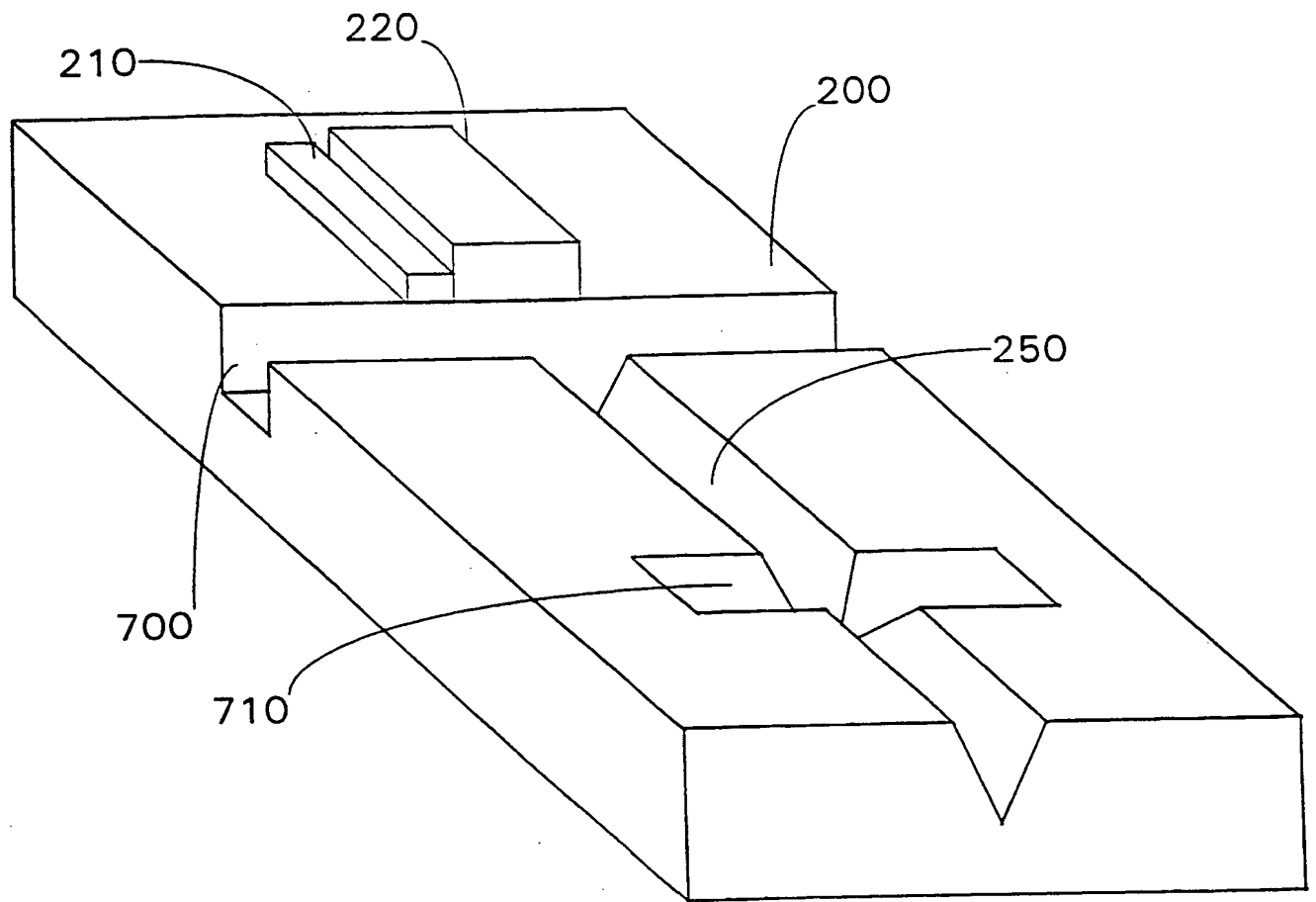


Fig.7.

8/8

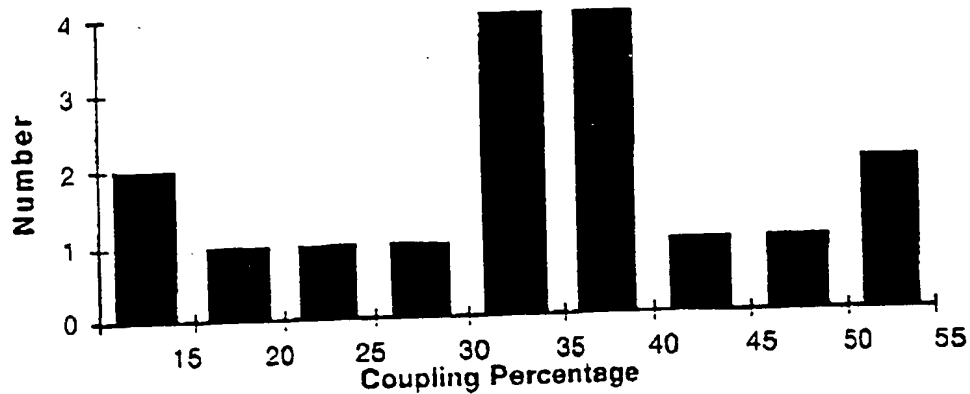


Fig.8.

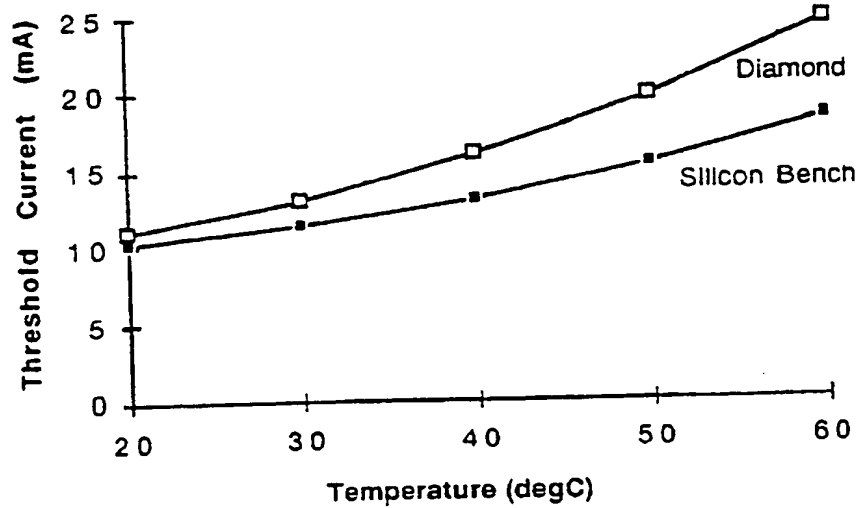


Fig.9.

## INTERNATIONAL SEARCH REPORT

National Application No

PCT/GB 95/01542

A. CLASSIFICATION OF SUBJECT MATTER  
IPC 6 G02B6/42

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)  
IPC 6 G02B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US,A,4 466 696 (CARNEY JAMES K) 21 August 1984 see figures ---	1,3,5,19
X	EP,A,0 466 134 (GTE LABORATORIES INC) 15 January 1992 see column 3, line 55 - column 4, line 47 ---	1,3
A	EP,A,0 419 767 (SIEMENS AG) 3 April 1991 see column 2, line 24-34 ---	1,3
A	DE-U-85 25 398 (SIEMENS) 15 December 1988 see claims; figures ---	1,3,5,23
A	EP-A-0 006 042 (THOMSON) 12 December 1979 see abstract; figure 1 ---	1,3,23
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☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

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Date of the actual completion of the international search

22 August 1995

Date of mailing of the international search report

13.09.95

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Fuchs, R

# INTERNATIONAL SEARCH REPORT

Int. Application No  
PCT/GB 95/01542

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT		
Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US-A-4 867 524 (D.P.COURTNEY ET AL.) 19 September 1989 see column 6, line 21-30; claim 1 ---	3,4,7
A	PATENT ABSTRACTS OF JAPAN vol. 6 no. 99 (E-111) ,8 June 1982 & JP,A,57 030394 (FUJITSU) 18 February 1982, see abstract ---	1-3
A	PATENT ABSTRACTS OF JAPAN vol. 10 no. 264 (P-495) ,9 September 1986 & JP,A,61 090108 (NEC) see abstract -----	14-16

## INTERNATIONAL SEARCH REPORT

International Application No

PCT/GB 95/01542

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EP-A-0419767	03-04-91	DE-D- 59003592 JP-A- 3146500 US-A- 5307433	05-01-94 21-06-91 26-04-94
DE-U-8525398	15-12-88	NONE	
EP-A-0006042	12-12-79	FR-A- 2426347 CA-A- 1164700 JP-A- 54150993 US-A- 4411057	14-12-79 03-04-84 27-11-79 25-10-83
US-A-4867524	19-09-89	DE-D- 68922451 EP-A- 0358592 JP-A- 2256007	08-06-95 14-03-90 16-10-90